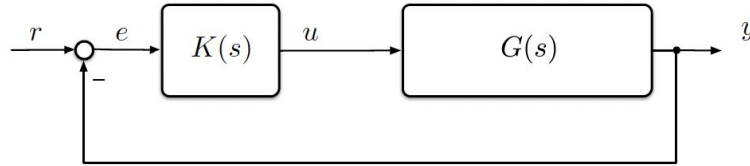


Review:
Closed Loop Stability &
Design Specifications

Dr. Keith Moffat

Classical control (Week 4)

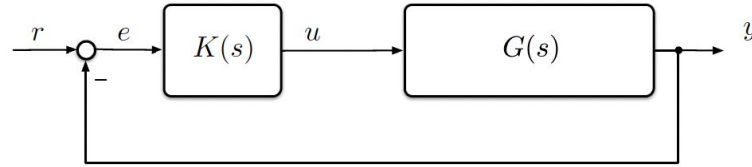


Known: $G(s)$

Desired: Good closed loop behavior (robust, etc.)

Approach: Choose $K(s)$ with as few calculations as possible

Classical control



Known: $G(s)$

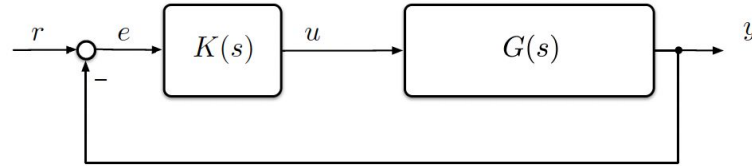
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We are interested in closed loop stability, but we design the open loop transfer function.

$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

Classical control



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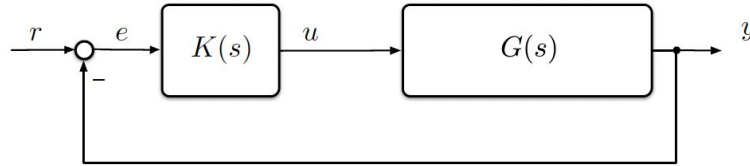
robust



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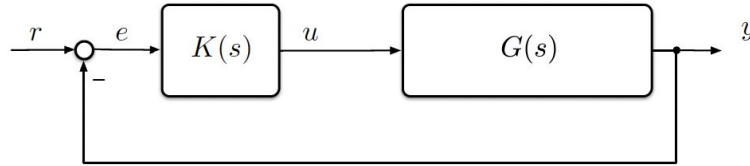
robust

We are interested in  closed loop stability, but we design the open loop transfer function.

$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

What do we want to be robust to?

Classical control



Known: $G(s)$

Desired: Good closed loop behavior (robust, etc.)

Approach: Choose $K(s)$ with as few calculations as possible

robust



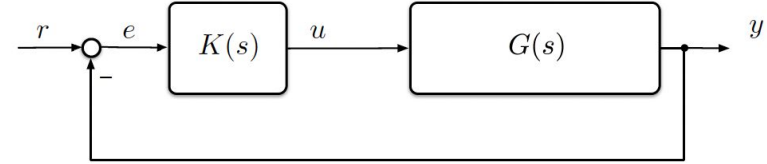
We are interested in closed loop stability, but we design the open loop transfer function.

$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

What do we want to be robust to?

- Model mismatch
- Delay
- Disturbances and measurement noise

Robust closed loop stability

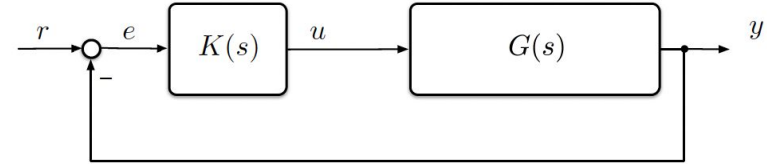


Given an open loop transfer function KG ,
we can determine the closed-loop stability by looking at the closed loop transfer function.

$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

But this doesn't help us *design* robust controllers.

Robust closed loop stability



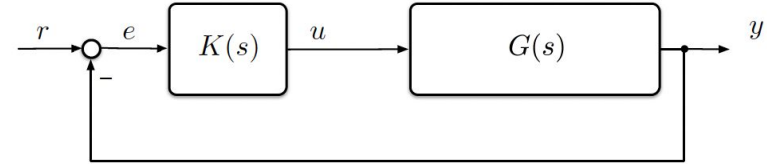
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Robust closed loop stability



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$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

But this doesn't help us *design* robust controllers.

To design robust controllers, we need some notion of how close the closed loop system is to instability.

The techniques we have covered

- Root Locus
- Nyquist
- Bode
- Small gain criterion

can be seen as robust design techniques.

Bode plots (Week 3)

Bode plots illustrate transfer functions

Why is the plot in log-log axes?

Signal magnitude factors are additive in the log scale: $\lg(a \cdot b) = \lg a + \lg b$

Why are Bode plots plotted in “decibels” (i.e. scaled by 20)?

Because that’s how they started doing it ~100 years ago

: 'bel' = signal energy in log-scale

$$|G|_{\text{dB}} = 10 \lg |G|^2 = 20 \lg |G|$$

Helpful resource: <https://lpsa.swarthmore.edu/Bode/BodeHow.html>

Less-helpful resource:

https://www.youtube.com/watch?v=QHPRrUTn5vQ&ab_channel=CarlosBodefan

Bode:



Bode skiing:



Bode plots

Bode plots illustrate the transfer function/frequency response of a system

Frequency response

The frequency response of a system is its magnitude and phase shift for every single-frequency input

Frequency response

The frequency response of a system is its magnitude and phase shift for every single-frequency input

Magnitude and phase shift can be represented in the separate magnitude and phase plots

→ Bode plots

Frequency response

The frequency response of a system is its magnitude and phase shift for every single-frequency input

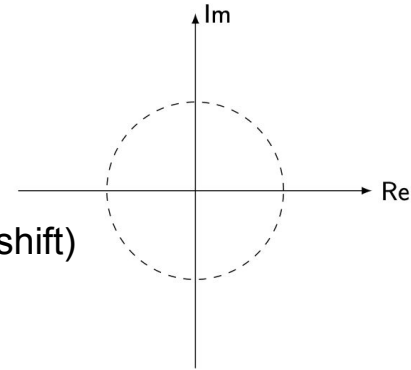
Magnitude and phase shift can be represented in the separate magnitude and phase plots

→ Bode plots

or

Magnitude and phase shift can be represented in a single complex plane plot ($j = 90^\circ$ shift)

→ Nyquist plots



Frequency response

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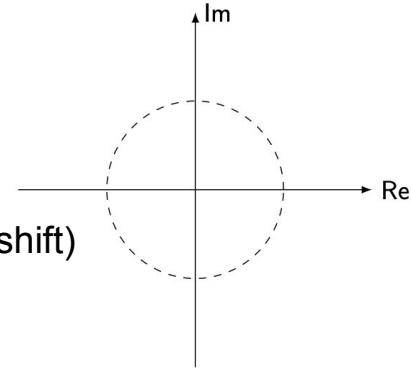
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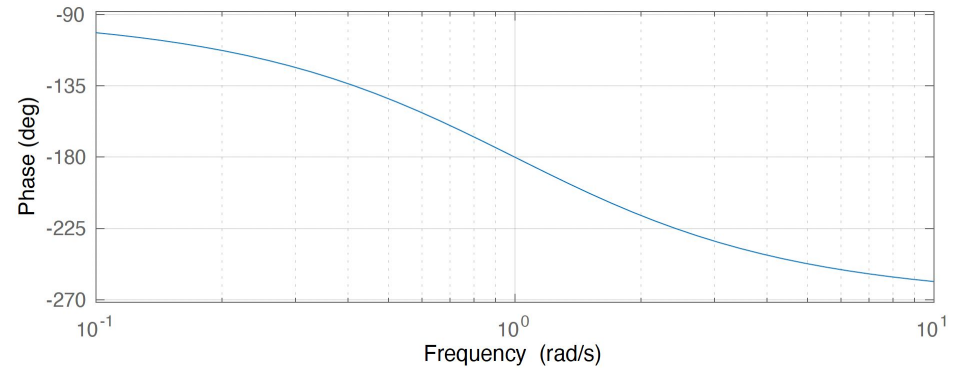
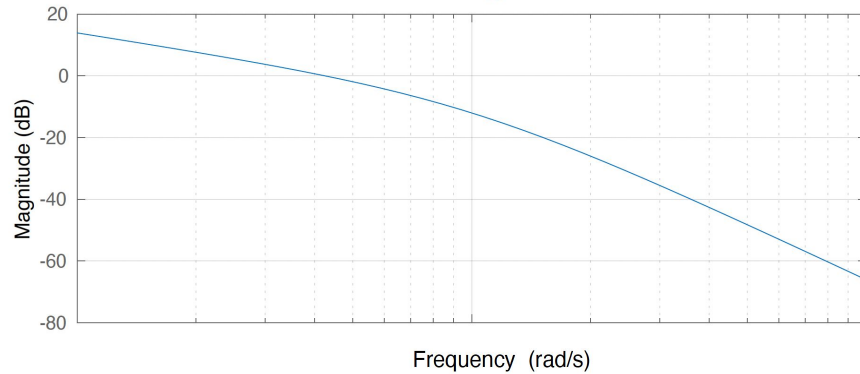
Replacing s in the transfer function with $j\omega$ gives you the frequency response equation: e.g. $G(j\omega)$

→ the Laplace transform gives you the frequency response

Bode plots

Bode plots illustrate the transfer function/frequency response of a system

→ Describe the gain and phase shift for the spectrum of all input frequencies in two separate plots

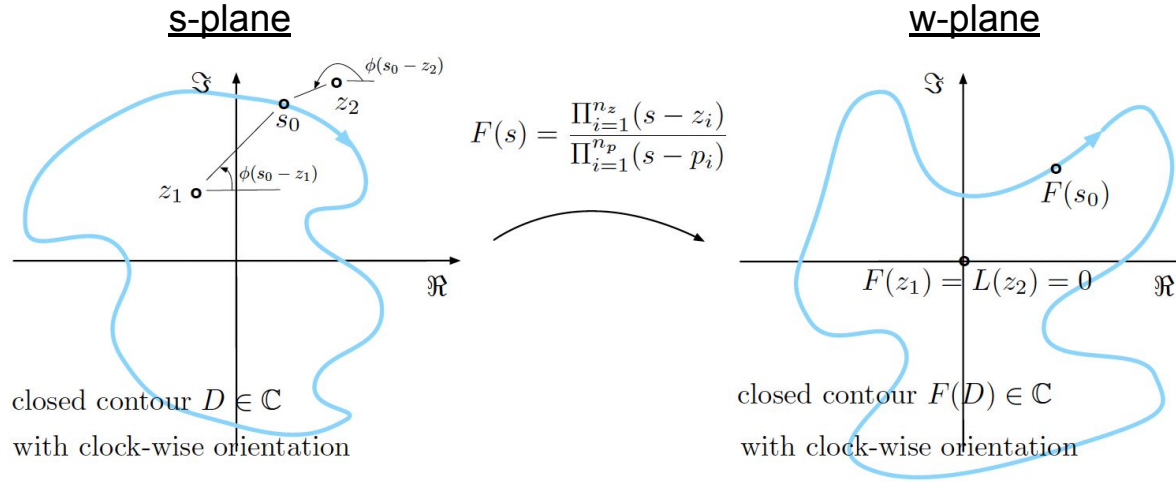


Nyquist plot

*Nyquist plots **also** illustrate the transfer function/frequency response of a system*

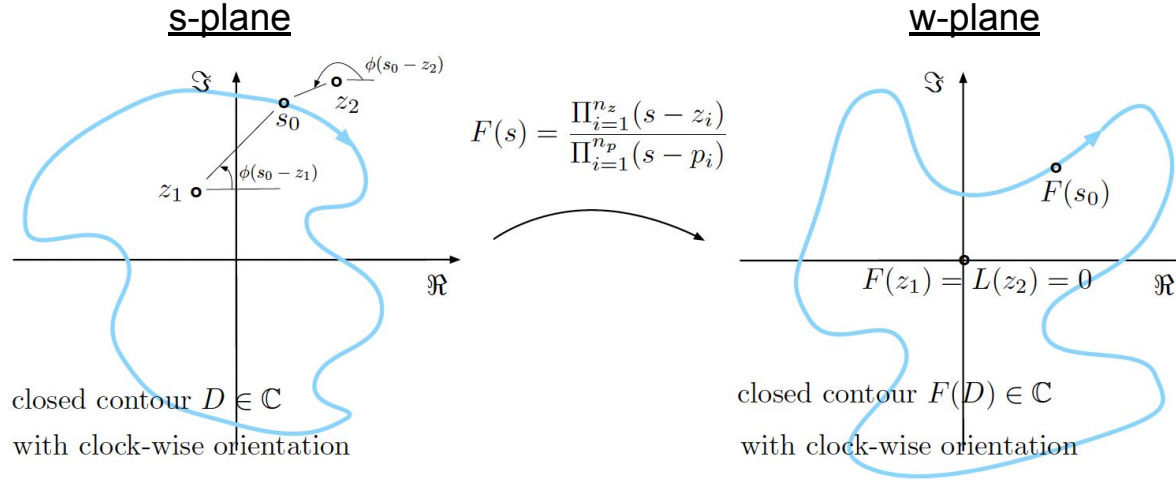
→ Describe the gain and phase shift for the spectrum of all input frequencies in a *single* plot

Cauchy's Argument Principle



$$\text{phase of } F(s) \text{ at } s_0 \in D = \underbrace{\sum_{i=1}^{n_z} \angle(s_0 - z_i)}_{\text{contribution of zeros}} - \underbrace{\sum_{j=1}^{n_p} \angle(s_0 - p_j)}_{\text{contribution of poles}}$$

Cauchy's Argument Principle



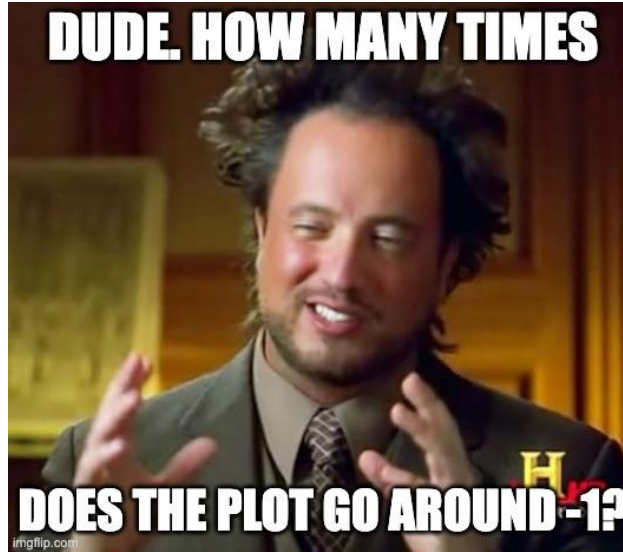
phase of $F(s)$ at $s_0 \in D = \underbrace{\sum_{i=1}^{n_z} \angle(s_0 - z_i)}_{\text{contribution of zeros}} - \underbrace{\sum_{j=1}^{n_p} \angle(s_0 - p_j)}_{\text{contribution of poles}}$

A seemingly useless observation...

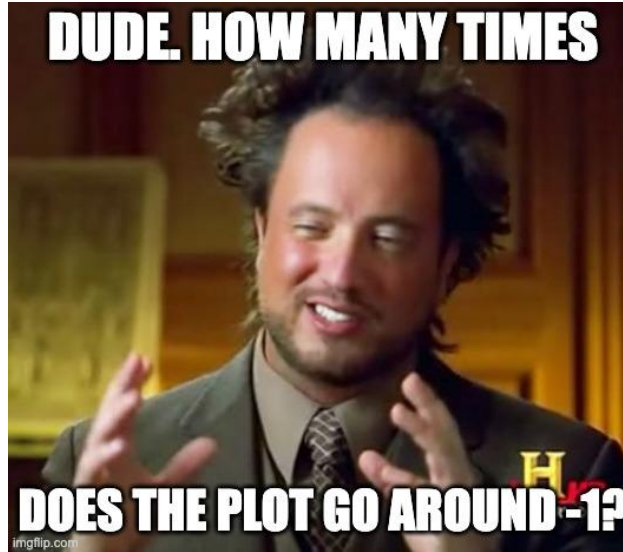
Why do we care?



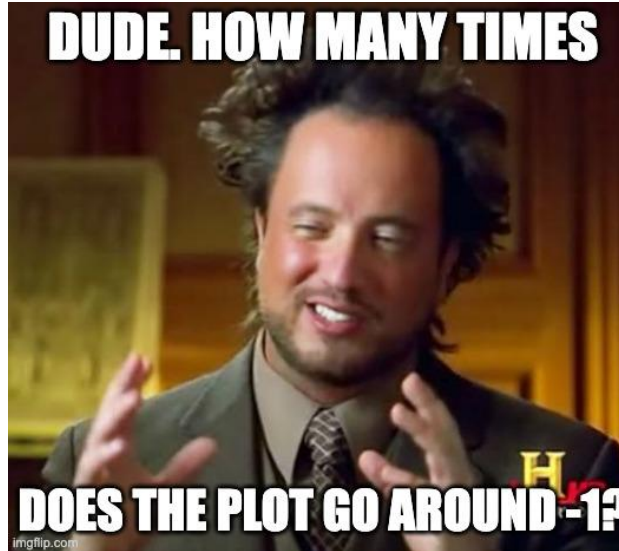
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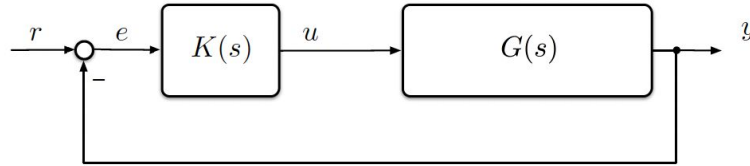
Why do we care?



WHAT PLOT, DUDE??
WHY DO WE CARE ABOUT -1???



Classical control



Known: $G(s)$

Desired: Good closed loop behavior (robust, etc.)

Approach: Choose $K(s)$ with as few calculations as possible

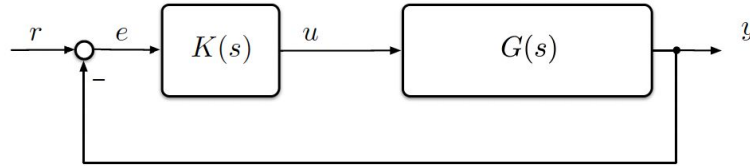
robust



We are interested in closed loop stability, but we design the open loop transfer function.

$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

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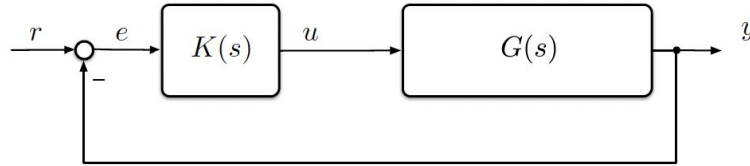
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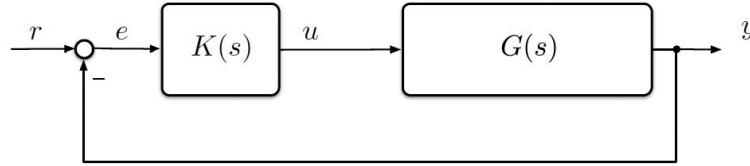
robust

We are interested in closed loop stability, but we design the open loop transfer function.

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These poles must be in the LHP

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robust

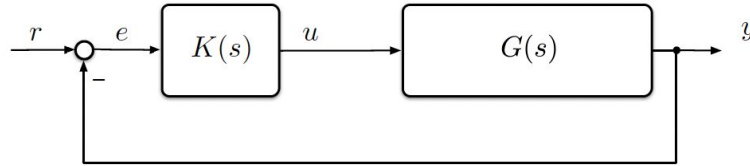
We are interested in closed loop stability, but we design the open loop transfer function.

$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

The zeros of $1+GK$
must be in the LHP

These poles must
be in the LHP

Classical control



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We are interested in closed loop stability, but we design the open loop transfer function.

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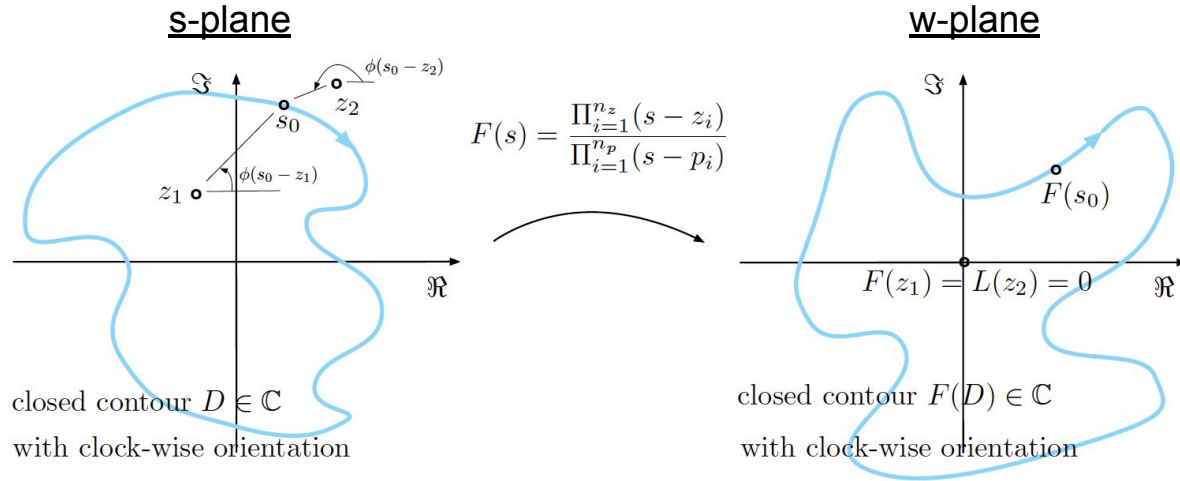
This is hard to determine
from inspection of GK

The zeros of $1+GK$
must be in the LHP

These poles must
be in the LHP

Cauchy's Argument Principle

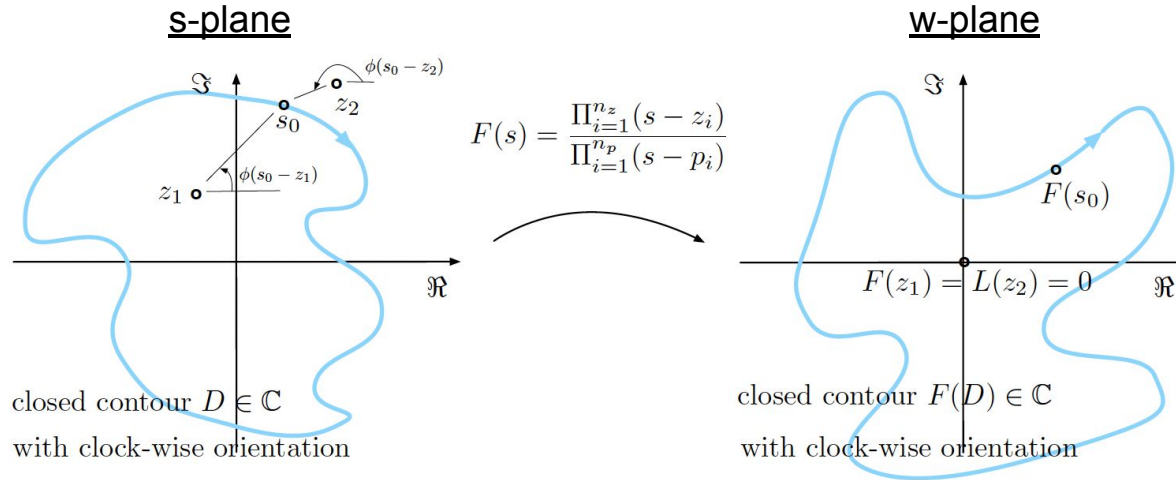
Tells you how many more poles than zeros are in a s-plane loop, based on how many times the w-plane loop encircles the origin in the counter-clockwise (CCW) direction.



A seemingly useless observation...

Cauchy's Argument Principle

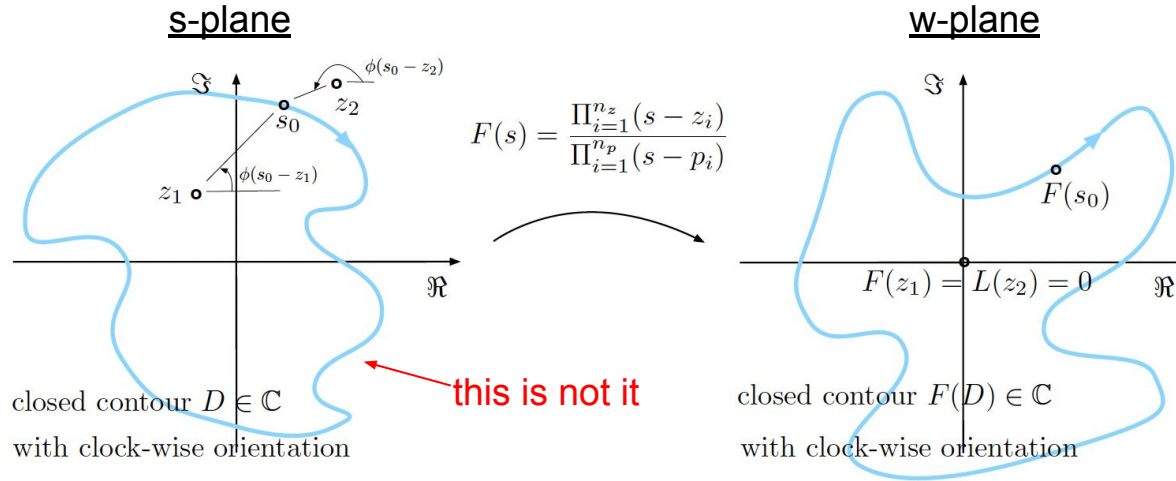
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A seemingly useless observation... turned out to be the foundation of classical control theory.

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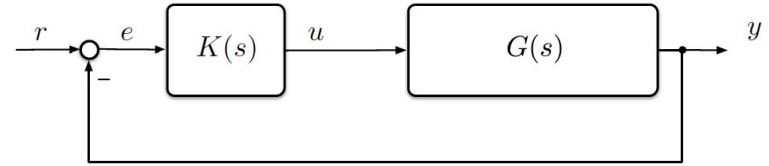
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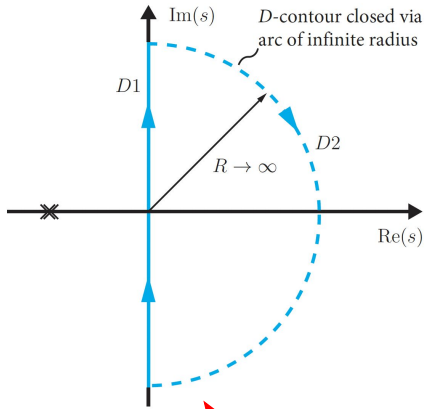
→ we have to choose the **right** s-plane contour

Nyquist Criterion



$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

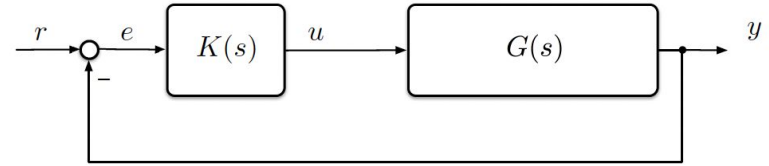
s-plane



this is the right s-plane contour (since we are interested in stability)

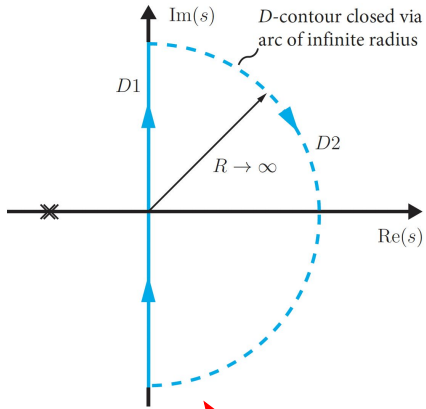
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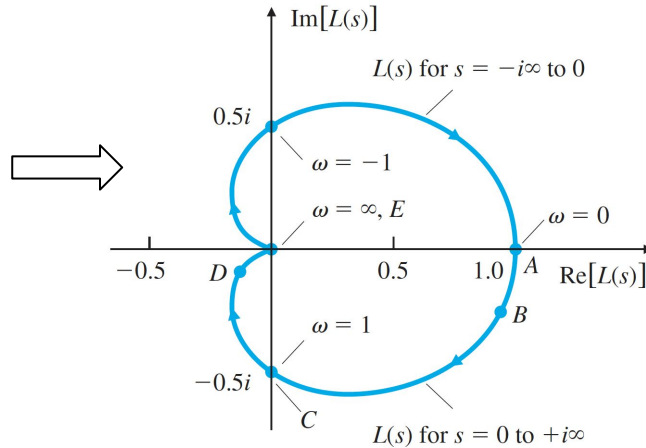


$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

s-plane



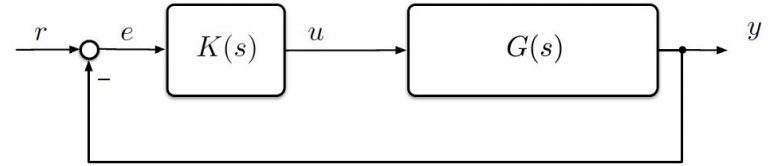
w-plane



this is the right s-plane contour (since we are interested in stability)

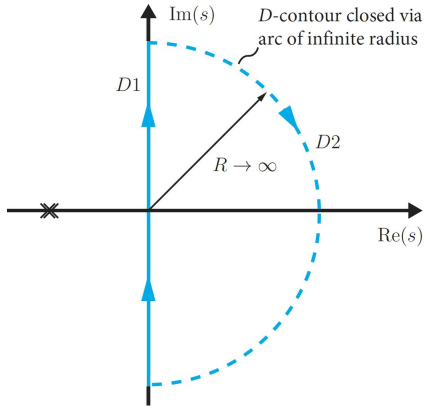
→ we have to choose the **right** s-plane contour

Nyquist Criterion

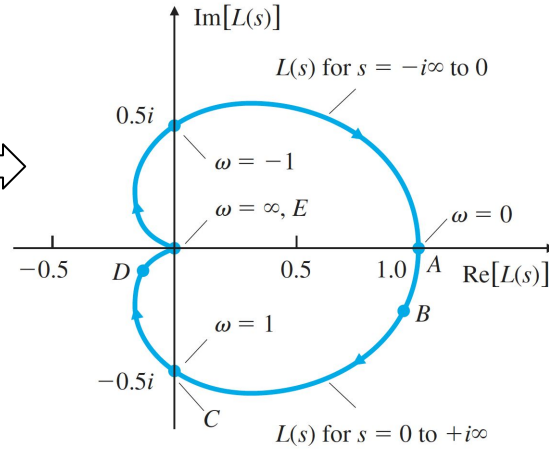


$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

s-plane

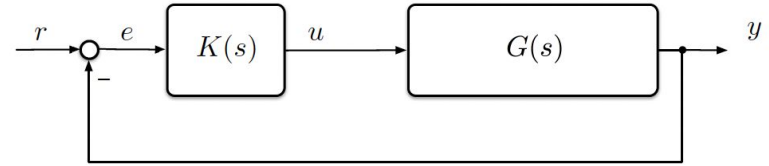


w-plane



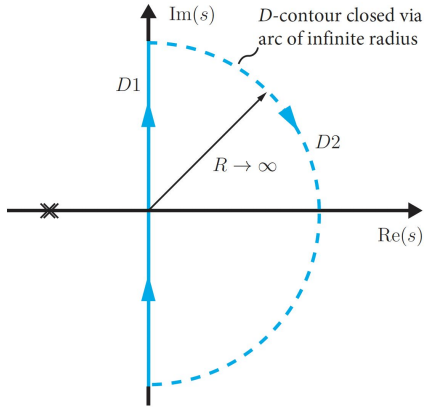
We are interested in the zeros of $1 + GK$
→ encirclements of -1, not 0

Nyquist Criterion

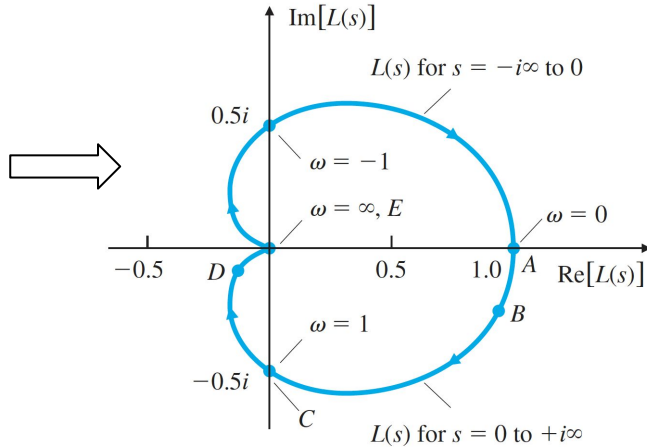


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s-plane



w-plane

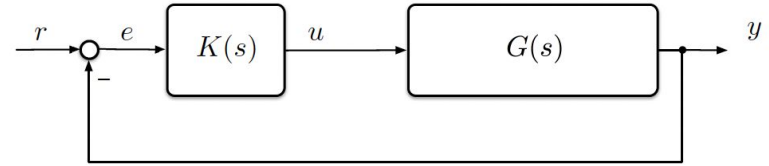


⇒ the closed-loop system is stable if and only if

$$N + P = 0$$

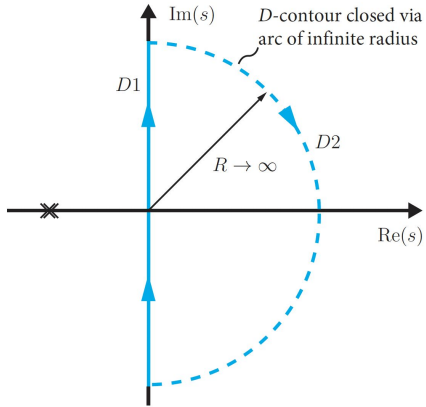
- N is the number of clockwise (CW) encirclements of -1
- P is the number of open loop poles in the RHP

Nyquist Criterion

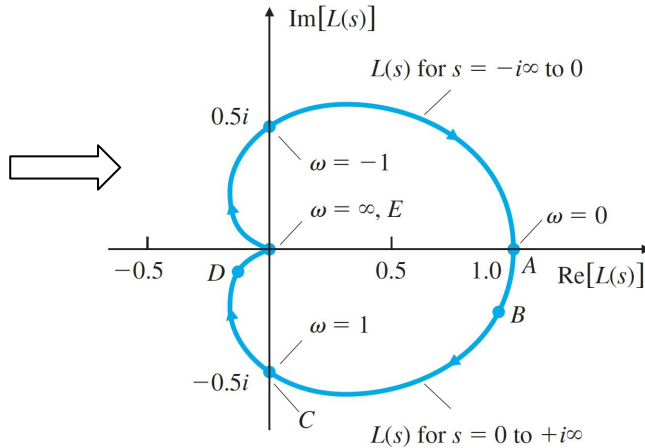


$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

s-plane



w-plane



⇒ the closed-loop system is stable if and only if

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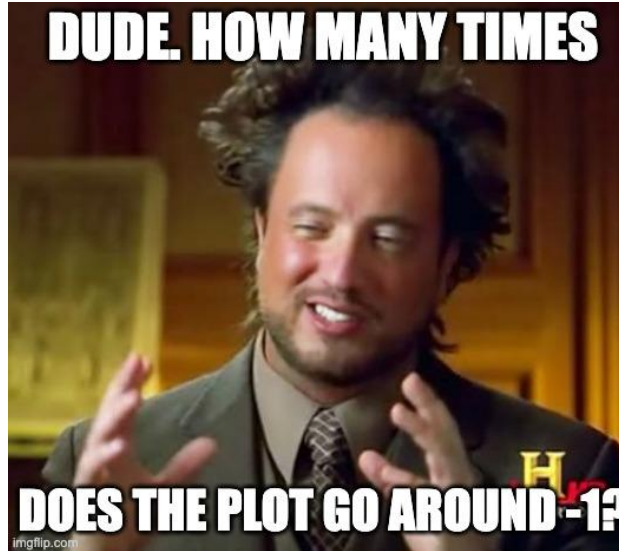
Need 1 CCW encirclement of -1 for each pole of GK in the RHP

Nyquist Criterion Implementation

1. Determine the number of OL poles in the RHP (the poles of GK are the poles of $1 + GK$)
2. Draw/use python to display the Nyquist Diagram of GK
3. Count net CCW encirclements of -1
(a CW encirclement cancels out a CCW encirclement)

→ If the net CCW encirclements of -1 = # OL poles in the RHP, the close loop system is stable.

Why do we care?



WHAT PLOT, DUDE??
WHY DO WE CARE ABOUT -1???

THE W-PLANE CORRESPONDING TO THE D-CONTOUR.
-1 ENCIRCLEMENT TELL US ABOUT CL STABILITY!

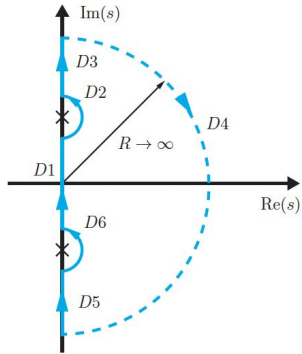
Nyquist Plot, poles on imag. axis

What if there are poles on the imaginary axis?



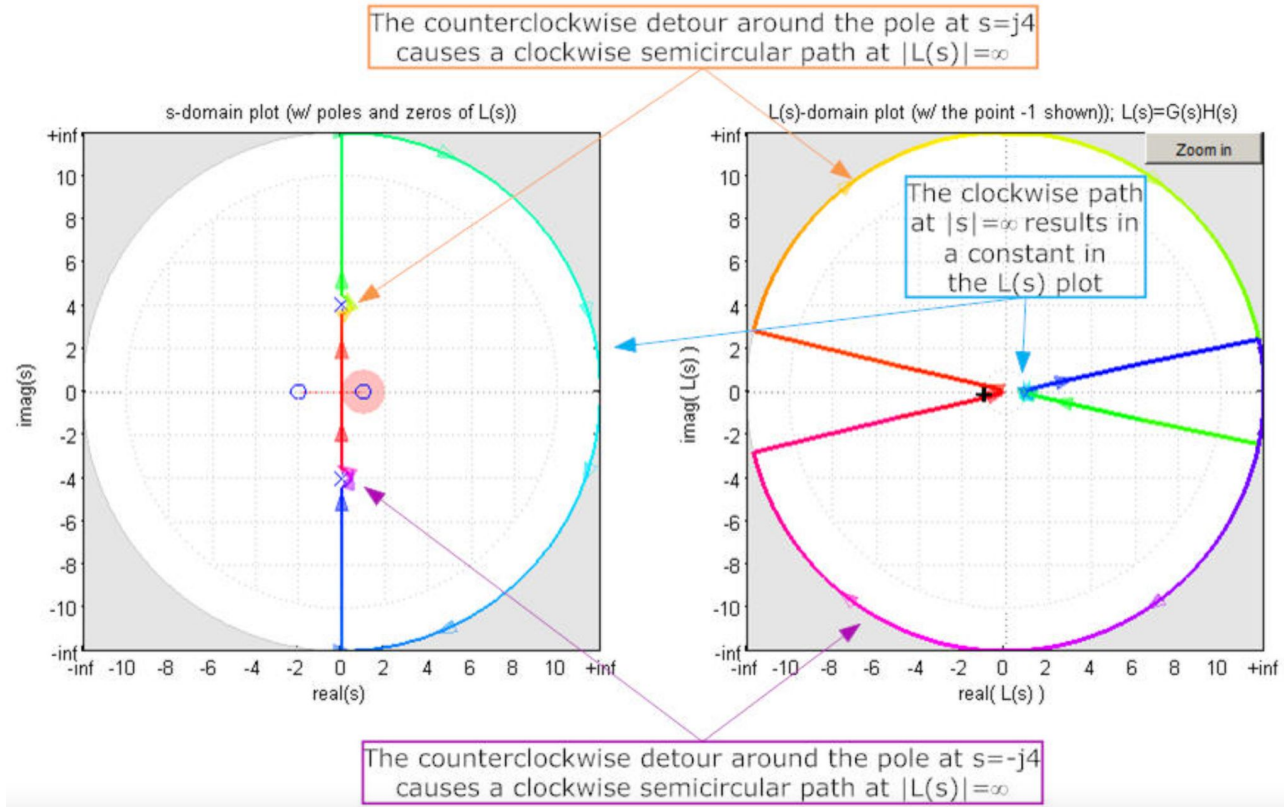
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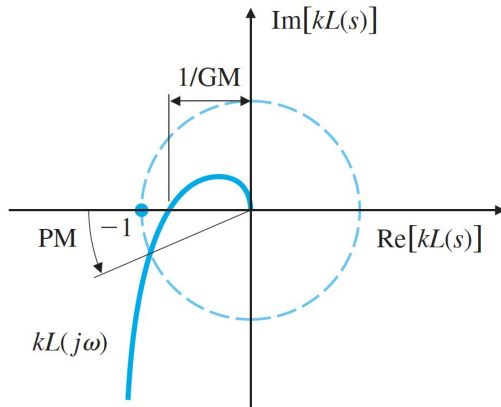
The detour arcs $D2$ and $D6$ are mapped to half-circles in the w -plane with infinity radius

Nyquist Plot, poles on imag. axis



Gain and phase margins, Nyquist

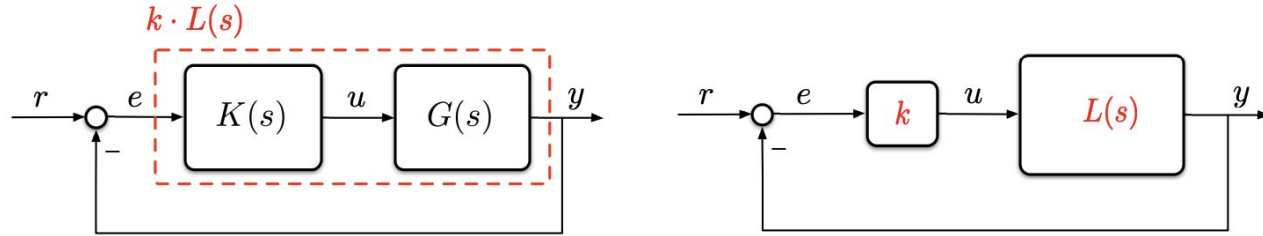
Nyquist



- phase margin
 \approx robustness against time delays
- gain margin
 \approx robustness against uncertainty in gain

are two measurements of robustness.

Nyquist Criterion, admissible gains

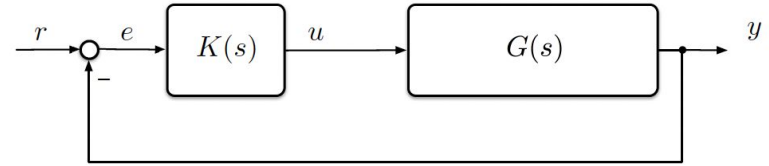


shifted & scaled map of D via $L(s) = \frac{F(s)}{k} - \frac{1}{k}$
= map of D via $F(s)$ shifted by $(-1/k, 0)$ and scaled by $1/k$

count encirclements of $-1/k$ via $L(s)$

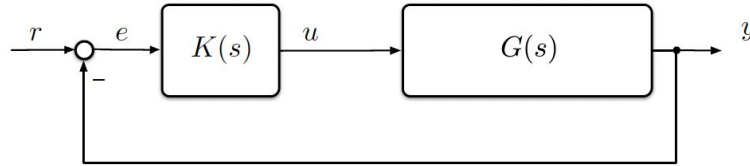
useful to find range of admissible control gains k

Bode Criterion



Unlike the Nyquist Criterion, the Bode criterion applies only if the OL does not have RHP poles

Classical control



Known: $G(s)$

Desired: Good closed loop behavior (robust, etc.)

Approach: Choose $K(s)$ with as few calculations as possible

robust



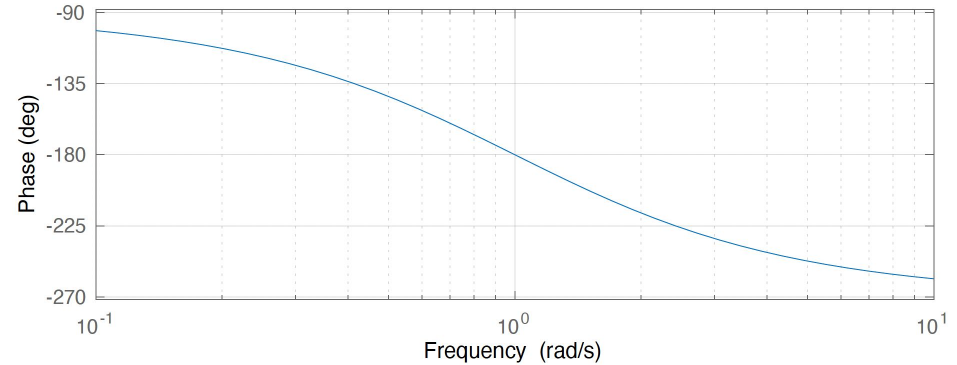
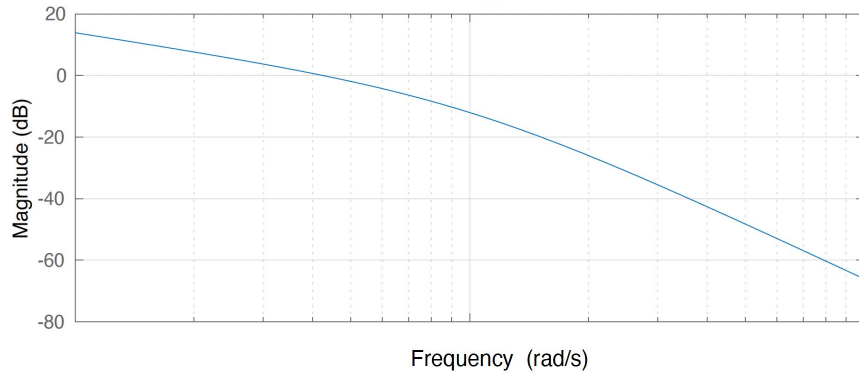
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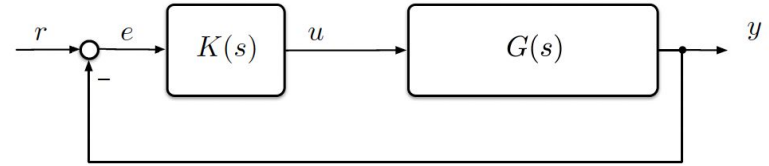
Bode plots

Bode plots illustrate the transfer function/frequency response of a system

→ Describe the gain and phase shift for the spectrum of all input frequencies

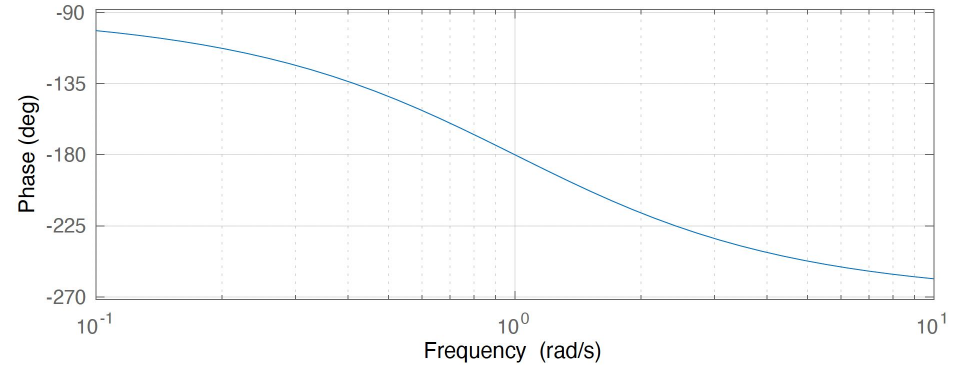
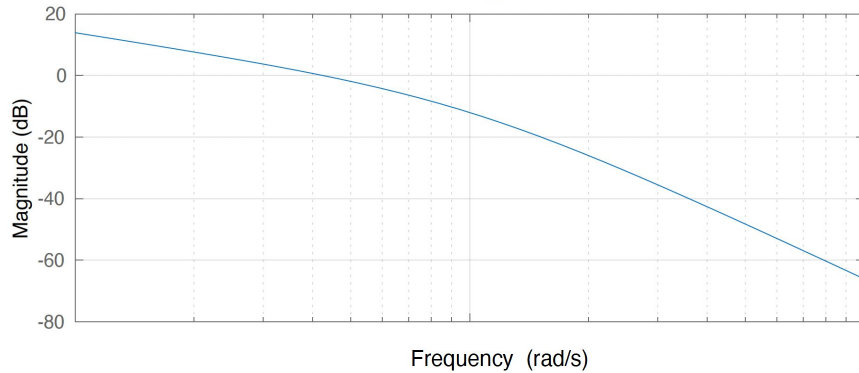


Bode Criterion



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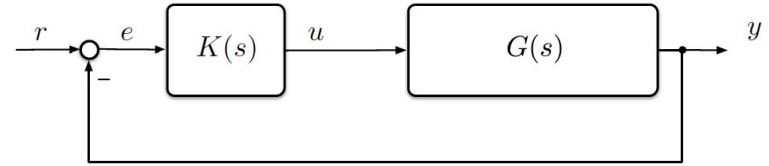
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Can we determine the stability of the closed loop system from the open loop Bode plot?

$$\frac{y(s)}{r(s)} = \frac{GK}{1 + GK}$$

Bode Criterion



Bode plots illustrate the transfer function/frequency response of a system

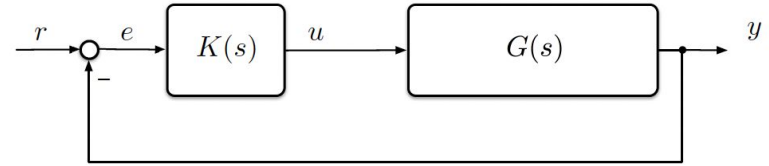
→ Describe the gain and phase shift for the spectrum of all input frequencies

From Nyquist Criterion:

If the OL does not have RHP poles, then the CL is stable when the Nyquist diagram does not encircle -1

→ guaranteed if $|GK| < 1$ when the phase crosses -180° (and $|GK|$ stays less than 1)

Bode Criterion



Bode plots illustrate the transfer function/frequency response of a system

→ Describe the gain and phase shift for the spectrum of all input frequencies

From Nyquist Criterion:

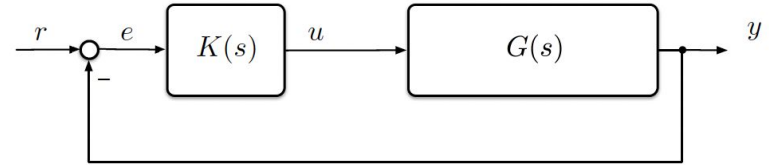
If the OL does not have RHP poles, then the CL is stable when the Nyquist diagram does not encircle -1

→ guaranteed if $|GK| < 1$ when the phase crosses -180° (and $|GK|$ stays less than 1)

Bode Criterion (applies to open-loop stable/no OL RHP pole systems):

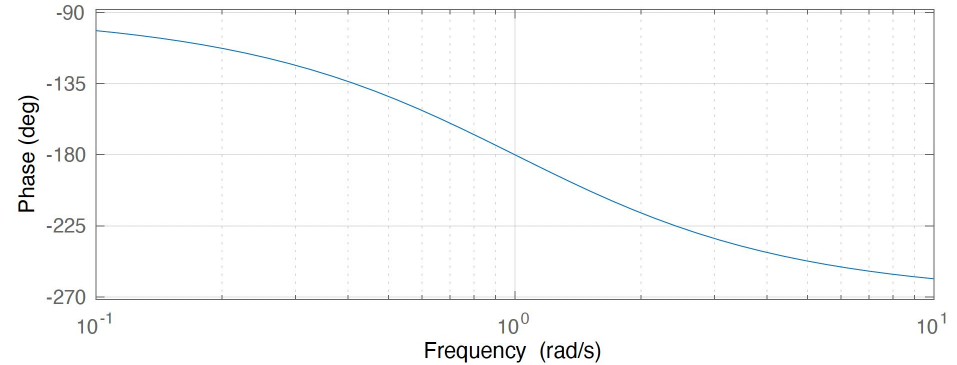
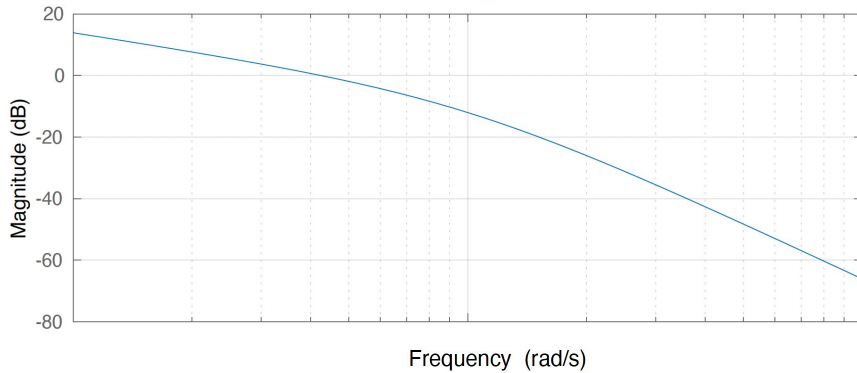
→ *The CL system is stable if the gain is less than 1 (0 dB) when the phase crosses -180°*

Bode Criterion



Bode plots illustrate the transfer function/frequency response of a system

→ Describe the gain and phase shift for the spectrum of all input frequencies

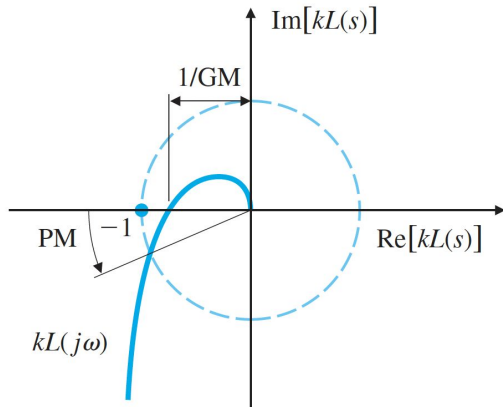


Bode Criterion (applies to open-loop stable/no OL RHP pole systems):

→ *The CL system is stable if the gain is less than 1 (0 dB) when the phase crosses -180°*

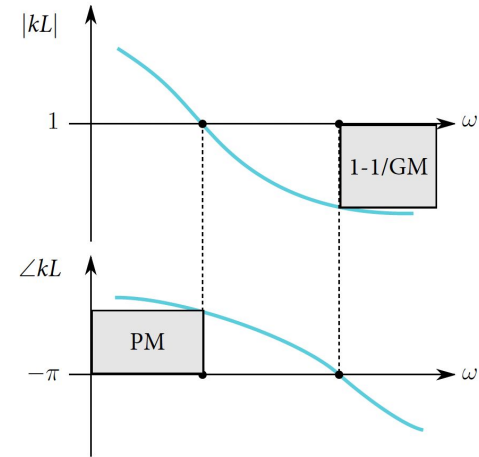
Gain and phase margins

Nyquist



- phase margin
 \approx robustness against time delays
- gain margin
 \approx robustness against uncertainty in gain

Bode



are two measurements of robustness.

Why do we care?

